	Polymer models	The critical endpoint pulling force	Pushing at the top	
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# Models of pulled and compressed polymers

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Combinatorial Applications to Biology, Chemistry and Physics University of Saskatchewan, Saskatoon 21-22 June 2014

## Collaborators

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Outline			

# Introduction

- Self-avoiding walks
- Generating functions

## 2 Polymer models

- Pulling and pushing
- Including a surface interaction

# The critical endpoint pulling force

- Overview
- Self-avoiding bridges
- Decompositions
- Divergence of generating functions
- Further results

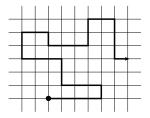
## Pushing at the top

Pushing Dyck paths



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Self-avoiding	g walks			

A self-avoiding walk (SAW) is a walk on a lattice which cannot revisit vertices.



For a given lattice,  $c_n$  is the number of *n*-step SAWs (up to translation). eg. square lattice:

$$c_0 = 1$$
  
 $c_1 = 4$   
 $c_2 = 12$   
 $c_3 = 36$   
 $c_4 = 100, \dots$ 

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# For regular lattices in $d \ge 2$ , no known expression for $c_n$ . But we still know something!

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For regular lattices in  $d \ge 2$ , no known expression for  $c_n$ . But we still know something!

Any SAW of length m + n can be split into two smaller SAWs, of lengths m and n. So

 $c_{m+n} \leq c_m c_n$ .

So  $\{c_n\}$  is a sub-multiplicative sequence. Then

 $\log c_{m+n} \leq \log c_m + \log c_m,$ 

so  $\{\log c_n\}$  is a sub-additive sequence. It follows that the limit

$$\log \mu = \lim_{n \to \infty} \frac{1}{n} \log c_n$$

exists.  $\log\mu$  is called the connective constant of the lattice. Then

$$c_n = \theta(n)\mu^n,$$

where  $\mu$  is called the growth constant (sometimes connective constant) and  $\theta(n) = e^{o(n)}$ . By submultiplicativity, we know that  $\theta(n) \ge 1$ .

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In general,  $\mu$  is not known exactly. Honeycomb lattice is special:

Theorem (Duminil-Copin and Smirnov 2012)

On the honeycomb (hexagonal) lattice,  $\mu = \sqrt{2 + \sqrt{2}}$ .

For other lattices, have numerical estimates based on series data (eg. 70 terms for square lattice)

 $\mu_{
m square} pprox 2.63815853031$   $\mu_{
m triangular} pprox 4.150797226$ 

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#### Subexponential factors unproven, but

# Conjecture (Nienhuis 1982)

$$c_n \sim An^{\gamma-1}\mu^n$$

for A,  $\mu$ ,  $\gamma$  constant. A and  $\mu$  are lattice-dependent,  $\gamma$  depends only on dimension. In two dimensions,  $\gamma = 43/32$ .

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#### Subexponential factors unproven, but

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In high dimensions, can do a bit better:

Theorem (Hara and Slade 1992)

On the hypercubic lattice in five or more dimensions,

 $c_n \sim A\mu^n$ .

Introduction	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Also interested in the size and shape of SAWs. eg. let  $\langle R_e^2 \rangle_n$  be the mean-squared end-to-end distance of SAWs of length *n*.

Conjecture (Nienhuis 1982; Lawler, Schramm and Werner 2004)

 $\langle R_e^2 \rangle_n \sim C n^{2\nu}$ 

with C lattice-dependent and  $\nu$  dimension-dependent. In two dimensions,  $\nu = 3/4$ .

The exponents  $\gamma$  and  $\nu$  are also connected to the scaling limit of SAWs:

Conjecture (Lawler, Schramm and Werner 2004)

Self-avoiding walks have a conformally invariant scaling limit, namely SLE<sub>8/3</sub>.

Introduction	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Generating	functions			

The (ordinary) generating function for  $\{c_n\}$  is

$$C(z)=\sum_{n\geq 0}c_nz^n$$

Then  $z_c = 1/\mu$  is the radius of convergence of C(z). In general, expect the behaviour near  $z_c$  to be

$$C(z) \sim ext{const.} (1 - z/z_c)^{-\gamma},$$

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Because  $c_n \ge \mu^n$ ,

$$C(z) \geq \sum_{n \geq 0} \mu^n z^n = \frac{1}{1 - z\mu}$$

So

$$C(z) o \infty$$
 as  $z o z_c^-$ .

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Expect that C(z) is non-D-finite, i.e. does not satisfy a linear ODE with polynomial coefficients.

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Polymer mo	odels			

SAWs are an important model in statistical mechanics of linear polymers in a solvent: chains of monomers, connected by bonds of fixed length and at fixed angles.

Unlike random walks (another, simpler model), SAWs encapsulate the excluded volume principle: two different monomers can't occupy the same point in space.

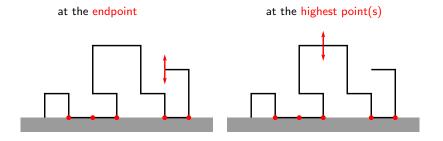
Monomers in a polymer can interact with each other, other polymers, surfaces (both penetrable and impenetrable) or with other external agents. Usually, these interactions are either attractive or repulsive.

Can also model forces applied to the polymer at various points/directions.

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Pulling ar	nd pushing			

We can model an external agent which is pulling the polymer away from the surface or pushing it onto the surface.

If one end of the polymer is tied to the surface, there are two natural places the force could be applied:



	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Force applie	d at the endpo	bint		

$$U_n^e(y) = \sum_h u_n^e(h) y^h.$$

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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$$U_n^e(y) = \sum_h u_n^e(h) y^h.$$

When y is small, walks whose endpoint is close to the surface dominate. When y is large, walks whose endpoint is far away from the surface dominate. So we can interpret  $y = e^{f}$ , where f is force: f > 0 if pulling up, f < 0 if pushing down.

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$$\lambda^{e}(y) = \lim_{n \to \infty} \frac{1}{n} \log U_{n}^{e}(y).$$

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For y > 0,  $\lambda^e(y)$  is

- convex in log  $y \iff$ continuous)
- non-decreasing

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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 $U_n^e(1)$  just counts walks in the upper half-plane.  $U_n^e(0)$  counts walks in the upper half-plane which start and end on the surface. Both of these have the same growth rate as full-plane walks, i.e.  $\mu$ . (Easy to show.)

So  $\lambda^e(0) = \lambda^e(1) = \log \mu \quad \Rightarrow \quad \lambda^e(y) = \log \mu \text{ for } 0 \leq y \leq 1.$ 

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 $\lambda^{e}(y) \geq \log y.$ 

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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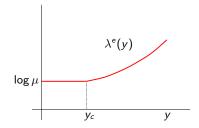
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So  $\lambda^e(y)$  must be non-analytic at some point  $y = y_c^e \ge 1$ . This is the critical point, where walks change from free to ballistic.



ndpoint pulling force Pushing at the top Future work	The critical endpoint pulling	Polymer models	
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## What does this really mean?

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Put a Boltzmann distribution on the walks of length n by setting

$$\mathbb{P}_n(\gamma) = \frac{y^{h(\gamma)}}{U_n^e(y)}$$

where  $h(\gamma)$  is the height of  $\gamma$ 's endpoint.

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Then the mean (endpoint) height per unit length for walks of length n is

$$\delta_n(y) = \frac{1}{n} \frac{\sum_h h u_n^e(h) y^h}{U_n^e(y)} = \frac{y}{n} \frac{\partial \log U_n^e(y)}{\partial y}$$

As  $n \to \infty$ , this becomes

$$\delta_n(y) \to y \frac{\partial \lambda^e(y)}{\partial y} \begin{cases} = 0 & \text{if } y < y_c \\ > 0 & \text{if } y > y_c. \end{cases}$$

So in the free phase, the average height of the endpoint is o(n), and walks "drift" away from the surface slowly. In the ballistic phase, the endpoint is at distance  $\Theta(n)$  from the surface.

(In the free phase, would expect the average height to grow like  $n^{\nu} = n^{3/4}$ .)

Induding a curfe as interaction						
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	Polymer models	The critical endpoint pulling force	Pushing at the top			

#### Including a surface interaction

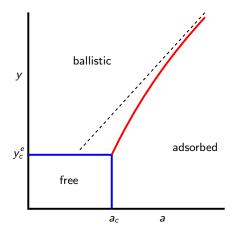
Can include a second fugacity *a* associated with returns to the surface. Then the surface can be repulsive (small *a*) or attractive (large *a*), and there is another critical value  $a_c$  which separates the two phases.



including a surface interaction

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Bivariate free energy  $\kappa^{e}(a, y)$ , which has critical points along several lines in the a - y plane.



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The critic	al endpoint pull	ing force		

#### Theorem

For the d-dimensional hypercubic lattice,  $d \ge 2$ , the critical value of the endpoint pulling fugacity is  $y_c^e = 1$ .

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The critic	The critical endpoint pulling force							

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The critic	The critical endpoint pulling force						

#### Theorem

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(It may also follow from some very technical probabilistic results of loffe and Velenik, but this remains unpublished.)

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Let  $\mu_u^e(y) = \exp(\lambda^e(y))$  be the growth rate of the partition functions  $U_n^e(y)$ , and

$$U^e(z,y) = \sum_n U^e_n(y) z^n$$

be the bivariate generating function with z conjugate to length and y conjugate to endpoint height.

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$$z_u^e(y) = \mu_u^e(y)^{-1}$$

is the radius of convergence of  $U^e(z, y)$ .

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So we need to show that the radius of convergence  $z_u^e(y)$  of  $U^e(z, y)$  is strictly decreasing for y > 1.

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Overview o	of proof			

The proof has four steps:

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Overview of	proof			

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- Find a relationship between the (bivariate) generating functions of four objects:
  - full-plane SAWs
  - half-plane SAWs
  - self-avoiding bridges
  - irreducible self-avoiding bridges

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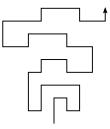
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- Show that this can only happen when the generating function of irreducible bridges is equal to 1.
- Show that the value of z solving this must decrease as y increases.

	Polymer models	The critical endpoint pulling force	Pushing at the top				
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Self-avoid	Self-avoiding bridges						

A self-avoiding bridge is a SAW  $\gamma = (\gamma_0, \gamma_1, \dots, \gamma_n)$ , where  $\gamma_i = (x_i^{(1)}, x_i^{(2)}, \dots, x_i^{(d)})$ , such that

$$x_0^{(d)} < x_i^{(d)} \le x_n^{(d)}$$
 for  $i = 1, \dots, n$ .

In 2 dimensions, a bridge is a SAW whose starting point has strictly minimal *y*-coordinate and whose end point has maximal *y*-coordinate:

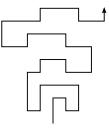


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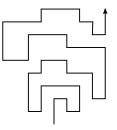
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Bridges are useful because they can be freely concatenated without intersecting.

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Irreducible b	oridges			

A bridge which cannot be split into a concatenation of two or more smaller bridges is irreducible:



Growth constants etc. are well-defined for bridges and irreducible bridges, and are the same as full-plane and half-plane walks, ie.  $\mu$ .

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Decompositions				

We already have the generating function  $U^e(z, y)$  for upper half-plane walks, with z tracking length and y tracking endpoint height.

Define B(z, y) and I(z, y) for bridges and irreducible bridges. (Endpoint and uppermost point are the same thing.)

Finally, introduce  $C^{e}(z, y)$  for full-plane SAWs. Because the endpoint can be lower than the starting point, the coefficient of  $z^{n}$  is a Laurent polynomial in y.

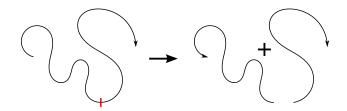
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Use well-known existing decompositions, but have to account for the second variable y.

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Use well-known existing decompositions, but have to account for the second variable y.

Any full-plane SAW can be split into two half-plane SAWs, with the direction of one reversed:

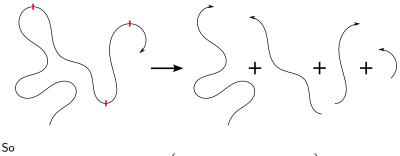


Thus

$$C^{e}(z,y) \leq U^{e}(x,y)U^{e}(x,1/y)$$

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Every half-plane SAW can be decomposed as a sequence of bridges which alternate direction and decrease in height:



$$U^e(z,y) \leq \prod_{h\geq 1} \left(1+(y^h+y^{-h})\sum_{n\geq 1}b_n(h)z^n\right)$$

where  $b_n(h)$  is the number of bridges of length *n* and height *h*.

Using  $1 + x \le e^x$ , get

$$U^{\mathsf{e}}(z,y) \leq e^{B(z,y)+B(z,1/y)}$$

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Combining,

$$C^{e}(z,y) \leq e^{2(B(z,y)+B(z,1/y))}$$

Finally, since every bridge can be written uniquely as a concatenation of irreducible bridges, we have

$$B(z,y) = \frac{I(z,y)}{1-I(z,y)}$$

	Polymer models	The critical endpoint pulling force	Pushing at the top			
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Divergence of generating functions (sketch)						

$$C^e_{m+n}(y) \leq C^e_m(y)C^e_n(y)$$

so  $C_n^e(y) \ge \mu^e(y)^n$  where  $\mu^e(y) = z_c^e(y)^{-1}$ .



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Then for  $y \ge 1$ ,  $U^e(z, y)$  must have the same critical point  $z_u^e(y) = z_c^e(y)$ , and diverge there. The same then goes for B(z, y). (In both cases it's not the 1/y function, because both  $U^e(z, y)$  and B(z, y) are strictly increasing in y.)

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But the only way that B(z, y) can diverge is if I(z, y) = 1.

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Divergenc	e of generating	functions (sketch)		

$$C^e_{m+n}(y) \leq C^e_m(y)C^e_n(y)$$

so  $C_n^e(y) \ge \mu^e(y)^n$  where  $\mu^e(y) = z_c^e(y)^{-1}$ .

Then for  $y \ge 1$ ,  $U^e(z, y)$  must have the same critical point  $z_u^e(y) = z_c^e(y)$ , and diverge there. The same then goes for B(z, y). (In both cases it's not the 1/y function, because both  $U^e(z, y)$  and B(z, y) are strictly increasing in y.)

But the only way that B(z, y) can diverge is if I(z, y) = 1.

 $I(z, y) = zy + 2z^6y^2 + O(z^7)$  is strictly increasing with y. So as y increases beyond y = 1, the solution to I(z, y) = 1 must decrease.

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So  $z_c^e(y) = z_u^e(y)$  is strictly decreasing for y > 1, and hence  $y_c^e = 1$ .

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Further resu	lts			

Can further complete the picture by relating the critical points for the different objects in the y < 1 and y > 1 regimes.

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Values of the critical exponents have been conjectured for some objects in some regimes: full- and half-plane walks for all values of y, bridges for  $y \ge 1$ .

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Pushing a	t the top			

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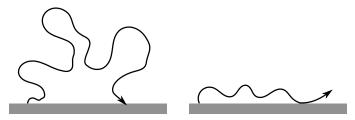
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When y < 1, however, things are very different:

pushing at end

pushing at top



Introduction 000000	Polymer models 000000	The critical endpoint pulling force	Pushing at the top O●OOOO	

When pushing at the endpoint, both ends must be near the surface but the rest of the walk has a lot of freedom.

 $\Rightarrow$  different critical exponent for y < 1, y = 1 and y > 1.

When pushing at the top, the whole walk must be near the surface.  $\Rightarrow$  much stronger restriction.

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Pushing at the top looks like restricting walks to a strip of finite height, so we might even expect the critical point (and hence the growth rate  $\mu_u^t(y)$ ) to change.

But walks with large height, even though they are heavily penalised, still contribute enough to keep the growth rate at constant  $\mu$ .

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Numerical series analysis suggests that for y < 1,

$$U_n^t(y) \sim A(y) n^{\gamma'-1} \mu^n \tau(y)^{n^{\sigma}},$$

where  $\tau(y) < 1$  and  $\sigma \approx 0.42$ .

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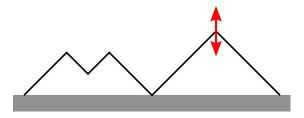
Similar for bridges when y < 1.

Resembles the conjectured asymptotics for collapsing partially directed walks (there,  $\sigma = 1/2$ ) [Brak, Owczarek, Prellberg 1993].

Introduction 000000	Polymer models 000000	The critical endpoint pulling force	Pushing at the top ○○○●○○	
Pushing Dyc	ck paths			

Try looking at a much simpler model to see if we observe the same behaviour.

Dyck paths take north-east (1, 1) or south-east (1, -1) steps, start and end on the surface, and remain above the surface.



Use z to track half-length (length is always even) and y to track height, as before. Then the generating function D(z, y) can be computed in several ways.

Unfortunately, extracting detailed information from the generating function for y < 1 proves to be very difficult.

Polymer models	The critical endpoint pulling force	Pushing at the top	
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However, can use it to calculate the free energy  $\lambda^d(y)$  exactly:

$$\lambda^d(y) = \log\left( egin{cases} 4 & ext{if } y \leq 1 \ rac{(y+1)^2}{y} & ext{if } y > 1 \end{array} 
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For y > 1, the partition function is asymptotically

$$D_n(y)\sim rac{(y-1)^3}{y(y+1)^2}\cdot \left(rac{(y+1)^2}{y}
ight)^n$$

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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For y < 1, Robin Pemantle and Brendan McKay use the fact that Dyck paths become reflected Brownian bridges in the scaling limit. If the distribution of the heights tends to a Gaussian, this can be asymptotically approximated and integrated. They obtain

$$D_n(y) = A(y)n^{-5/6}4^n\tau(y)^{n^{1/3}}(1+O(n^{-1/3})),$$

where

$$A(y) = (1 - y)2^{5/3}3^{-1/2}\pi^{5/6}e^{2r}$$
  
$$\tau(y) = \exp(-3 \times 2^{-2/3}\pi^{2/3}r^{2/3})$$

and  $r = -\log y$ .

Matches numerical analyses of 2500-term series.

Further asymptotic terms can be calculated using the same method.

	Polymer models	The critical endpoint pulling force	Pushing at the top	Future work
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Future work				

Complete the phase diagram picture for endpoint pulling when surface  $a \neq 1$ . Is it really the same for top-pulling?

On the honeycomb lattice,  $a_c$  is known exactly. Can other parts of the phase diagram be calculated exactly?

What kind of singularity leads to the y < 1 asymptotics for top-pushed SAWs and Dyck paths? Results are known for  $\tau^{n^{\sigma}}$  when  $\tau > 1$ , but we have  $\tau(y) < 1$ .

This can all be repeated with a penetrable surface. Still have  $y_c^e = 1$ , but the surface weight *a* is quite different.

	Polymer models	The critical endpoint pulling force	Pushing at the top	
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Thank you!